

2026

ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

Historical Record: 07/24/2026
External Version



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ATTENTION:

- The contents held within this book are for field maintenance only. Every effort should be made, when possible, to upgrade to current standards.

IF YOU HAVE ANY QUESTIONS REGARDING THE CONTENT OF THESE MANUALS, PLEASE EMAIL
CONSTRUCTIONSTANDARDSADMINISTRATORS@SEMPRAUTILITIES.COM OR CONTACT:

MANUAL	CONTACT	EMAIL ADDRESS	PHONE
Electric Distribution Design Manual	Fidel Castro	FRCastro@sdge.com	(858) 654-1607
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Service Standards & Guide	Jennifer Mann	jmann@sdge.com	(619) 676-1680
Electric Vehicle Supply Equipment Standards	Jennifer Mann	jmann@sdge.com	(619) 676-1680
Underground Construction Standards	Eddie Alcobia	ealcobia@sdge.com	(619) 574-4988
Electric Standard Practices	Joey Kucharyski	jkucharyski@sdge.com	(760) 566-5919
Tool Catalog	Roy Guilao	rguilao@sdge.com	(760) 672-6211

SUMMARY OF CHANGES

9/20/2024	NEW RELEASE, 6101, 6114, 6201, 6222	5	DMFMO2024v0920.pdf
2/21/2025	5201, 5223	2	DMFMO2025v0221.pdf
8/22/2025	6201, 6242	2	DMFMO2025v0822.pdf
11/21/2025	5401, 5431, 5432	3	DMFMO2025v1121.pdf
5/22/2026	6213	1	DMFMO2026v0522.pdf
7/24/2026	5701, 5745, 6101, 6134, 6136, 6201, 6241	7	DMFMO2026v0724.pdf

**5000
GENERAL
INFORMATION**

**5000
GENERAL
INFORMATION**

5000 - No FMO standards for this section.

5100
OVERHEAD LAYOUT
SYSTEMS

5100
OVERHEAD LAYOUT
SYSTEMS

5100 - No FMO standards for this section.

**5200
UNDERGROUND
LAYOUT SYSTEMS**

5200
UNDERGROUND
LAYOUT SYSTEMS

SUBJECT

5223

SINGLE FAMILY RESIDENTIAL SECONDARY SYSTEMS

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REV	CHANGE	DR	BY	DSN	APV	DATE	REV	CHANGE	DR	BY	DSN	APV	DATE			
C							F									
B							E									
A	ORIGINAL ISSUE	JKI	KNM	FRC	KRG	02/13/2025	D									
SHEET 1 OF 1			Indicates Latest Revision				Completely Revised			X	New Page			Information Removed		FMO DM5201
		SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY														
		TABLE OF CONTENTS UNDERGROUND LAYOUT SYSTEMS														

DM5223 FIELD MAINTENANCE ONLY

ALL VERSIONS LISTED IN FMO ARE SUPERSEDED BY THEIR CURRENT VERSION FOUND INSIDE THE ELECTRIC DISTRIBUTION DESIGN MANUAL.

REVISION HISTORY:

02/21/2025: DM5223 MOVED TO FMO

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REV	CHANGE	DR	BY	DSN	APV	DATE	REV	CHANGE	DR	BY	DSN	APV	DATE			
C							F									
B							E									
A	6114 MOVED TO FMO	JIK	KNM	FRC	KRG	02/13/2025	D									
SHEET 1 OF 1			Indicates Latest Revision				Completely Revised			X	New Page			Information Removed		FMO DM5223
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		SINGLE FAMILY RESIDENTIAL SECONDARY SYSTEMS														

This design standard provides the residential secondary and service system optimum array tables used in conjunction with the General Design Criteria provided in Design Manual 5222. These tables represent an economic analysis of secondary and service system design alternatives, on a cost per lot basis, for approximately 9600 different array possibilities.

The optimum array tables shall be used for residential single-family subdivision design to insure the lowest cost system is installed.

NONE

A. The optimum array tables provide the optimum array configuration, transformer size and secondary/service cable selections based on KW demand, secondary distance, and service distance. The instructions for properly applying the optimum array tables are as follows:

- Determine the KW demand per lot for the subdivision from the Residential Demand Estimating Criteria, Design Manual 5322.

- The secondary footage and structure (Transformer Pad or Handhole) placement is dictated by the lot front footage, street width, and meter location. Typically, the structures will be placed at the load center to serve as many meters as possible from one location. This requires the secondary footage to span from one to four lots or the street width. Therefore, the secondary footage is determined by:

- a. Measuring the distance across the number of lots being spanned or the distance across the street
- b. Adding footage to the overall distance for cable tools (Design Manual 5922). The typical secondary footage for a subdivision should be determined by measuring several lot combinations and using the most common footage(s) as a benchmark for optimum array selections.

- The service distance for a single-sided array service or double-sided array short service is equal to the service panel setback. The double-sided array long service is equal to the service panel setback plus the distance from the originating structure across the street to the property line. The service panel setback is either an estimated or measured distance from behind the sidewalk at the property line to the service panel location. Additional footage shall be added to this distance from the service cable tails (Design Manual 5922).

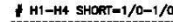
- Select the subdivision single-sided and/or double-sided optimum array configuration from the table with the appropriate KW demand, secondary and service lengths. The optimum array selection for the subdivision may be used for each individual array whose secondary and service footage does not differ from the typical by more than ten feet. Otherwise, an individual array selection must be made.

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C						F					
B	FORMATTING	JK	-	-	02/21/2020	E					
A	ORIGINAL ISSUE	-	CVN	RDG	01/01/1987	D					
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		SINGLE FAMILY RESIDENTIAL SECONDARY SYSTEMS									

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B	FORMATTING	JK	-	-	02/21/2020	E					
A	ORIGINAL ISSUE	-	CVN	RDG	01/01/1987	D					

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	SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY				
	SINGLE FAMILY RESIDENTIAL SECONDARY SYSTEMS				



Sq. Ft.: 2000-2999

SINGLE-SIDED

DOUBLE-SIDED

6.5KW EH & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

8KW A/C & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

DOUBLE-SIDED

7.5KW EH & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

7KW A/C & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

DOUBLE-SIDED

8KW EH & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

8KW A/C & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

DOUBLE-SIDED

8KW EH & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

8KW A/C & EWH

Sec

Fl

Serv

Fl

S1-S2

#

Cust

FMO
DM5223.7

**5300
DEMAND
ESTIMATING**

**5300
DEMAND
ESTIMATING**

5300 - No FMO standards for this section.

5400

VOLTAGE DROP

5400

VOLTAGE DROP

DM5431 FIELD MAINTENANCE ONLY

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11/06 /2025: MOVED TO FMO

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B							E						
A	5431 MOVED TO FMO	YZZ	FRC	FRC	FRC	11/06/2025	D						

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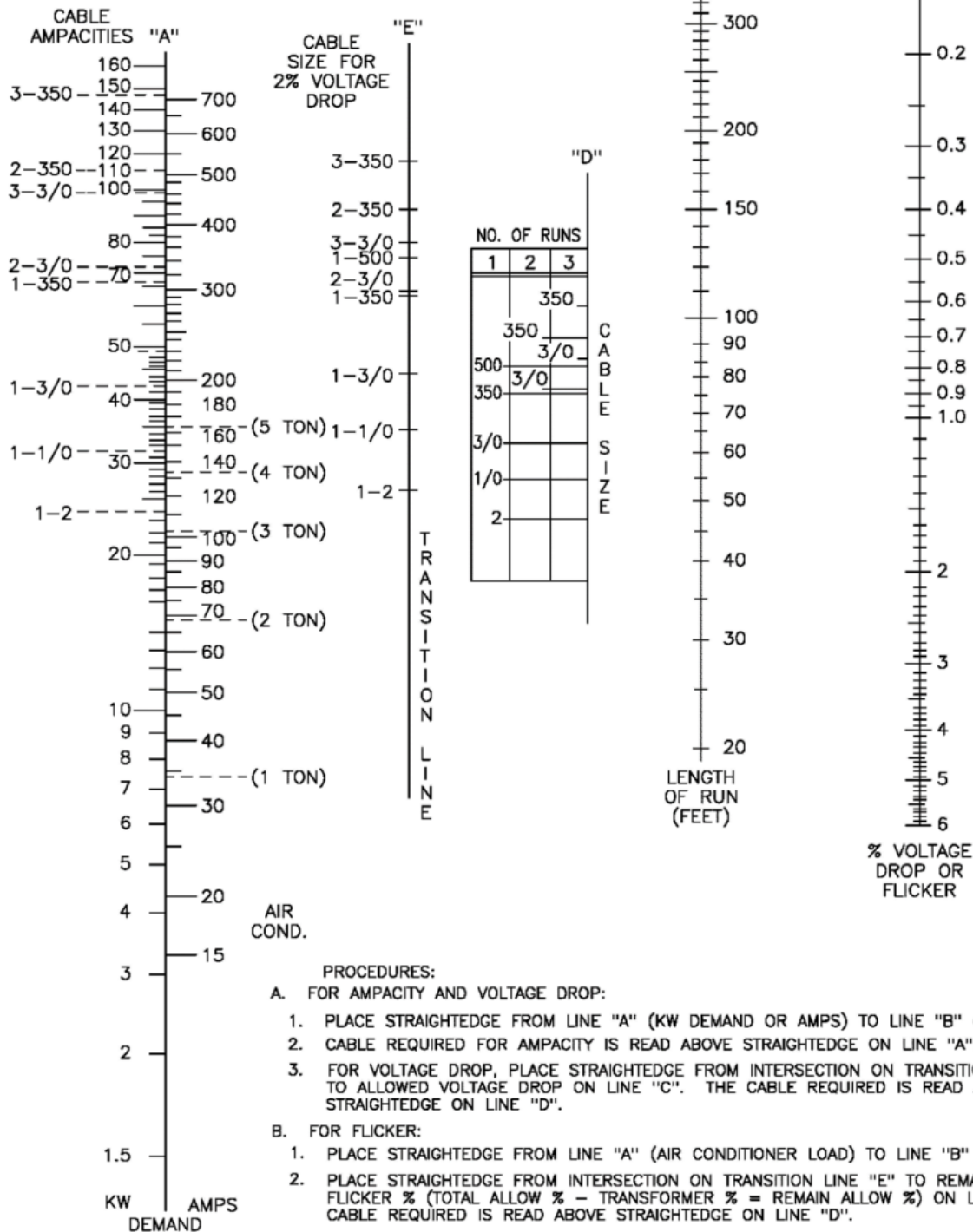
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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

UNDERGROUND VOLTAGE DROP AND FLICKER NOMOGRAPH

FMO
DM5431

SEE GENERAL NOTES ON PAGE 5413.3 IF THE % FLICKER IS GREATER THAN ALLOWABLE LIMITS.



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A	5431 MOVED TO FMO	YZZ	FRC	FRC	FRC	11/06/2025	D						

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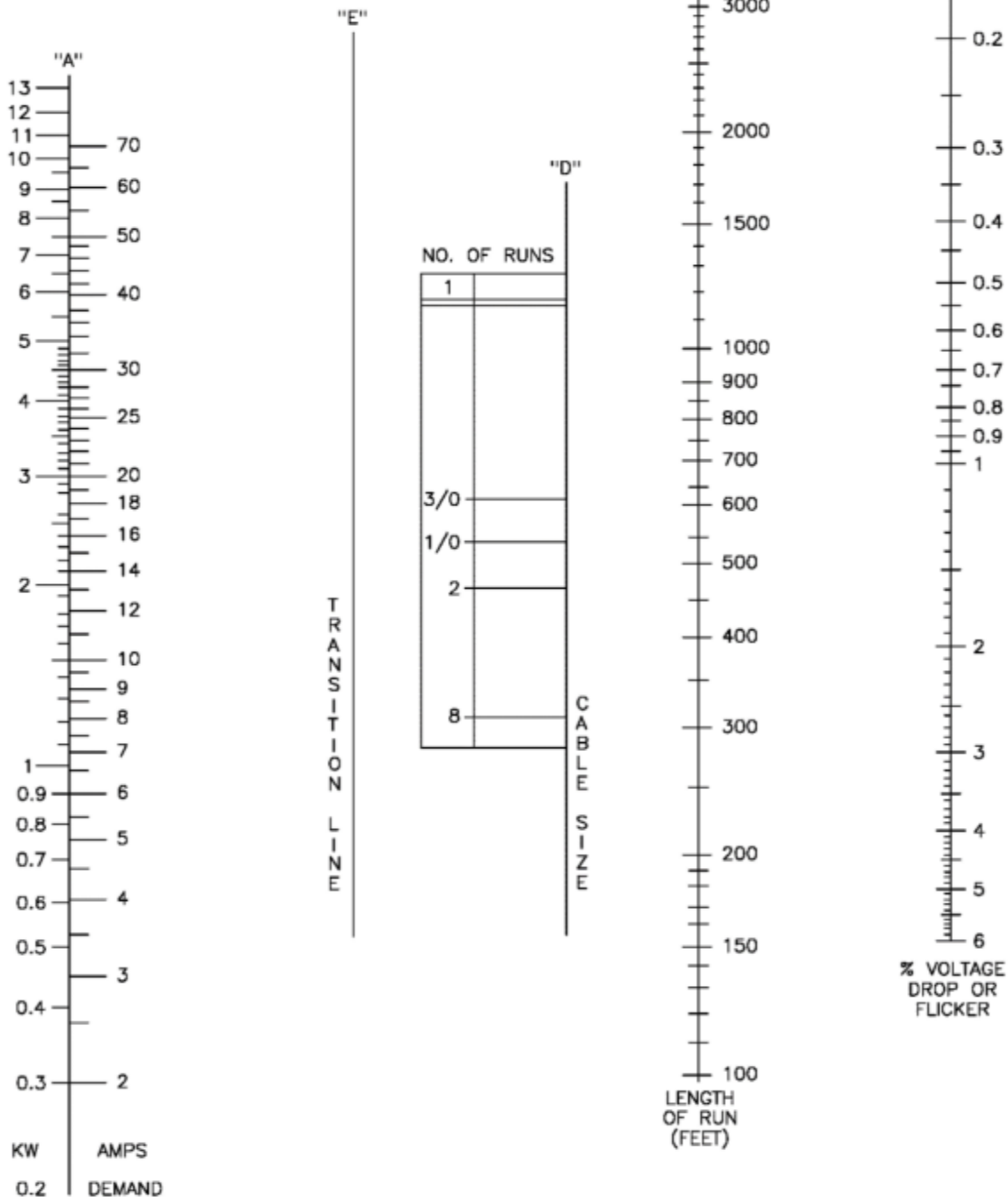
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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

SINGLE-PHASE 120/240V UNDERGROUND VOLTAGE DROP
AND FLICKER NOMOGRAPH

FMO
DM5431.1

PLACE STRAIGHTEDGE FROM KW DEMAND OR AMPS (LINE "A") TO LENGTH OF RUN (LINE "B"). THEN FROM THE TRANSITION POINT (LINE "E") TO THE SIZE OF CABLE (LINE "D"). READ THE % VOLTAGE DROP (LINE "C") FOR THAT SEGMENT OF CABLE.



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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

SINGLE-PHASE 120/240V UNDERGROUND STREET LIGHT NOMOGRAPH

FMO
DM5431.5

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	SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY					
	OVERHEAD VOLTAGE DROP AND FLICKER NOMOGRAPH					

PROCEDURES:

A. FOR AMPACITY AND VOLTAGE DROP:

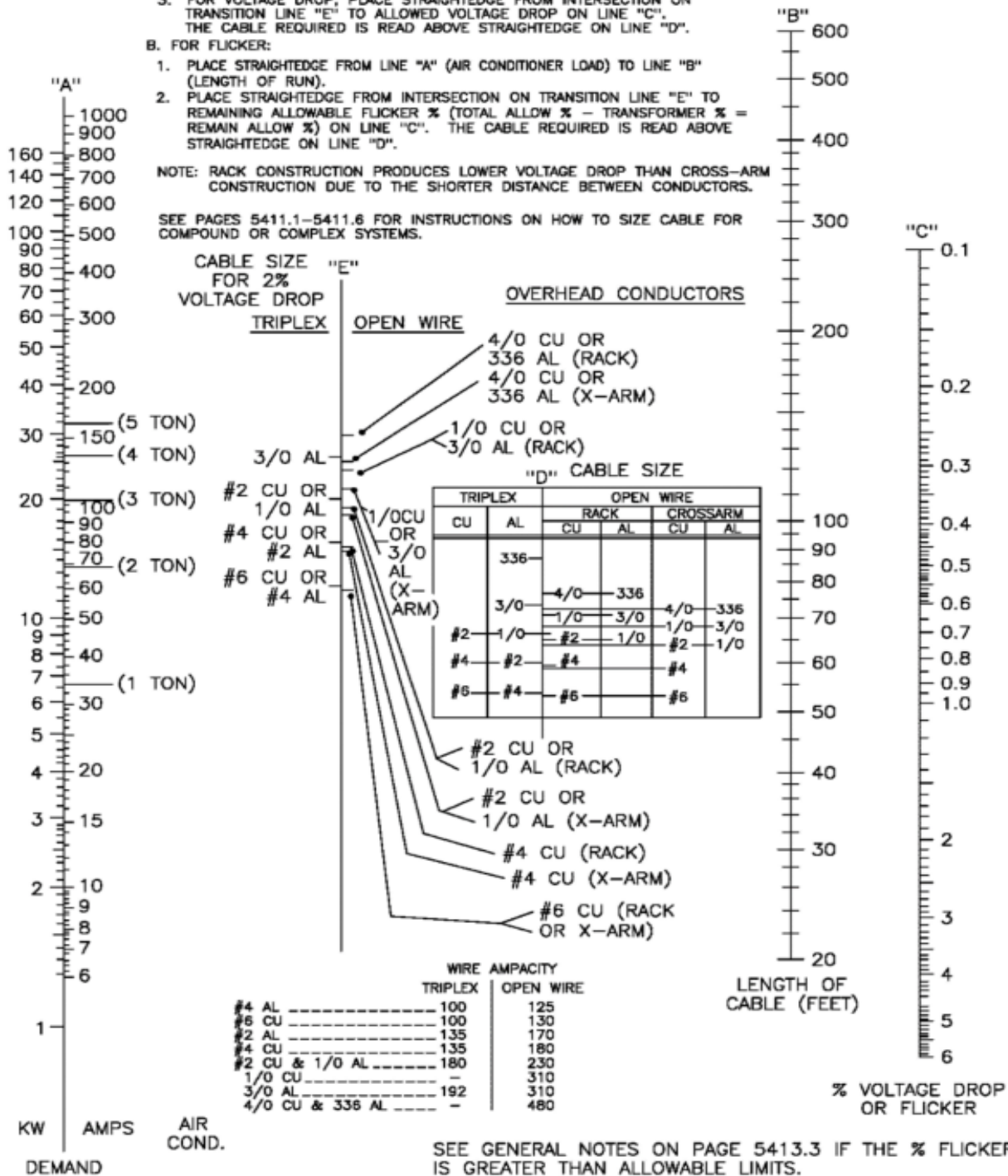
1. PLACE STRAIGHTEDGE FROM LINE "A" (KW DEMAND OR AMPS) TO LINE "B" (LENGTH OF RUN).
2. WIRE REQUIRED FOR AMPACITY IS READ OFF TABLE BELOW.
3. FOR VOLTAGE DROP, PLACE STRAIGHTEDGE FROM INTERSECTION ON TRANSITION LINE "E" TO ALLOWED VOLTAGE DROP ON LINE "C". THE CABLE REQUIRED IS READ ABOVE STRAIGHTEDGE ON LINE "D".

B. FOR FLICKER:

1. PLACE STRAIGHTEDGE FROM LINE "A" (AIR CONDITIONER LOAD) TO LINE "B" (LENGTH OF RUN).
2. PLACE STRAIGHTEDGE FROM INTERSECTION ON TRANSITION LINE "E" TO REMAINING ALLOWABLE FLICKER % (TOTAL ALLOW % - TRANSFORMER % = REMAIN ALLOW %) ON LINE "C". THE CABLE REQUIRED IS READ ABOVE STRAIGHTEDGE ON LINE "D".

NOTE: RACK CONSTRUCTION PRODUCES LOWER VOLTAGE DROP THAN CROSS-ARM CONSTRUCTION DUE TO THE SHORTER DISTANCE BETWEEN CONDUCTORS.

SEE PAGES 5411.1-5411.6 FOR INSTRUCTIONS ON HOW TO SIZE CABLE FOR COMPOUND OR COMPLEX SYSTEMS.



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A	5432 MOVED TO FMO	YZZ	FRC	FRC	FRC	11/06/2025	D						

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X New Page

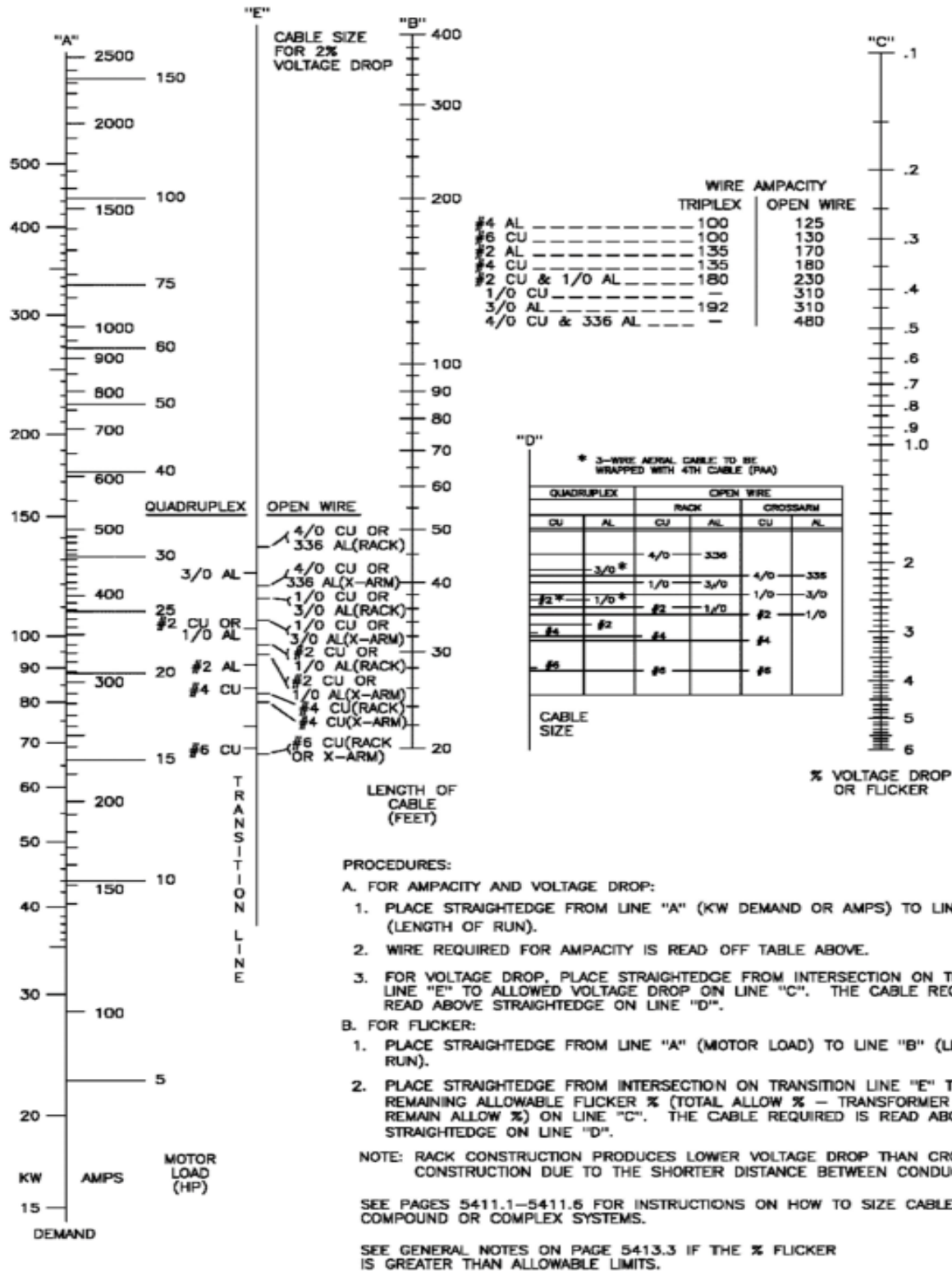
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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

SINGLE-PHASE 120/240V OVERHEAD VOLTAGE DROP
AND FLICKER NOMOGRAPH

FMO
DM5432.1



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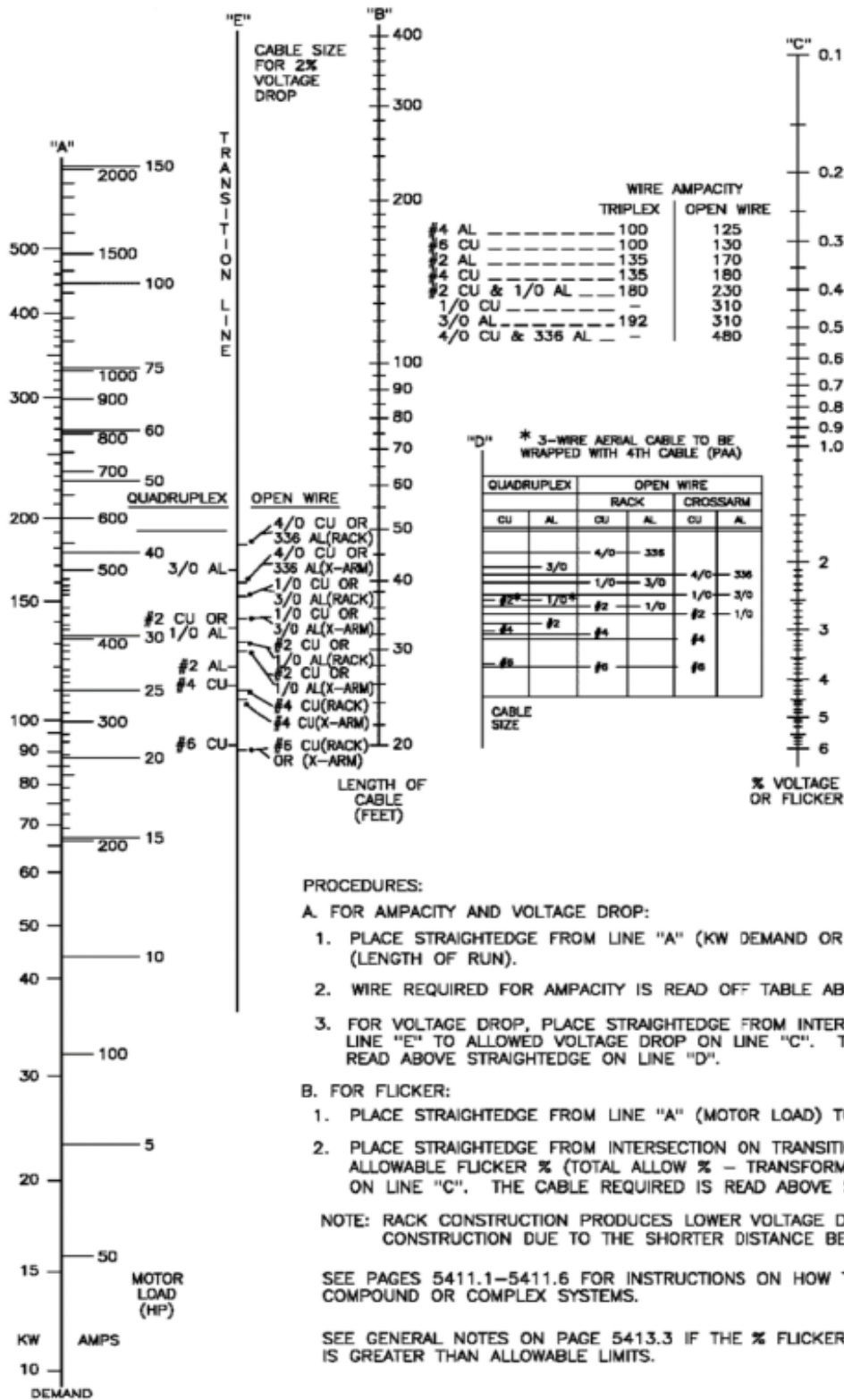
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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

THREE PHASE 120/208Y OVERHEAD VOLTAGE DROP
AND FLICKER NOMOGRAPH

FMO
DM5432.2



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C							F						
B							E						
A	5432 MOVED TO FMO	YZZ	FRC	FRC	FRC	11/06/2025	D						

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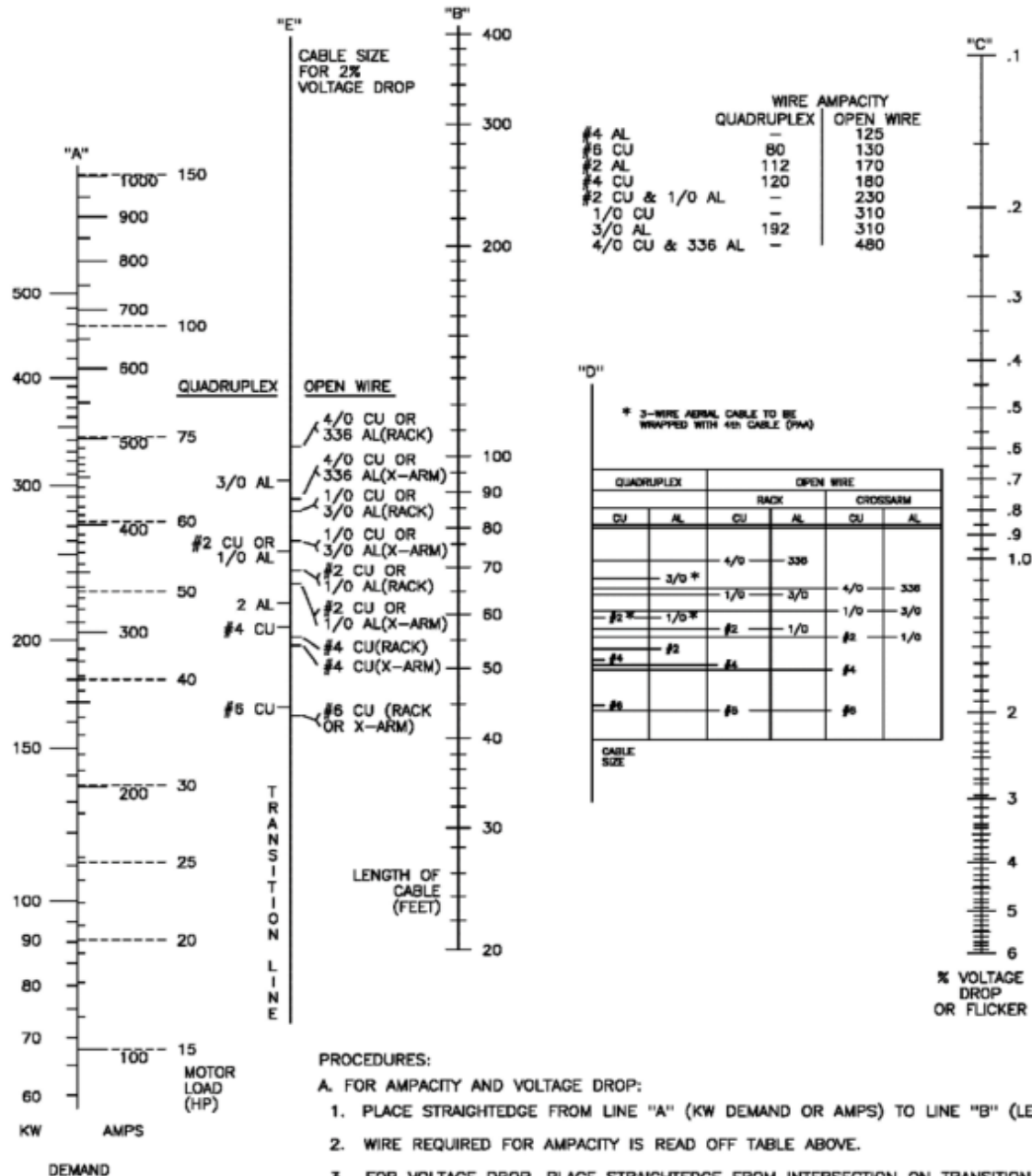
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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

THREE PHASE 120/240V OVERHEAD VOLTAGE DROP
AND FLICKER NOMOGRAPH

FMO
DM5432.3



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B							E						
A	5432 MOVED TO FMO	YZZ	FRC	FRC	FRC	11/06/2025	D						

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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

**THREE PHASE 480 OVERHEAD VOLTAGE DROP
AND FLICKER NOMOGRAPH**

**FMO
DM5432.4**

**5500
CONDUCTOR
AMPACITIES**

**5500
CONDUCTOR
AMPACITIES**

5500 - No FMO standards for this section.

5600

TRANSFORMERS

5600

TRANSFORMERS

5600 - No FMO standards for this section.

**5700
PADS &
SUBSTRUCTURES**

**5700
PADS &
SUBSTRUCTURES**

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1 OF 1

ELECTRIC VAULT DESIGN TABLES FOR SDG&E INTERNAL USE

FMO
DM5745

24.6. The following tables apply only to existing or legacy vaults. All new vault installations shall comply with DM5745, which requires a minimum floor-to-ceiling height of 12 feet.

24.6.1. Below grade single transformer vault requirements for 120/208V.

CUST. BOARD	208V TRANSF. SIZE	FRONT TO BACK*	WALL TO WALL	ALONG W/ TRANSF. SWITCH INSTALLED ON SIDE WALL.		ALONG W/ TRANSF. SWITCH INSTALLED ON END WALL		FLOOR TO CEILING	CEILING EQUIPMENT	TRANSF.	SUMP
SIZE	(KVA)	L LENGTH	W WIDTH	L LENGTH	W WIDTH	L LENGTH	W WIDTH	HEIGHT	OPENING	WEIGHT	CAP.
200	75	13' - 6"	9' - 6"	NA	NA	NA	NA	8' - 0"	4' - 6" X 6' - 6"	3,500	240
400	150	13' - 6"	9' - 6"	NA	NA	NA	NA	8' - 0"	4' - 6" X 6' - 6"	3,900	240
600	225	14' - 0"	9' - 6"	NA	NA	NA	NA	8' - 0"	5' - 0" X 6' - 6"	4,200	240
800	300	15' - 0"	10' - 6"	NA	NA	NA	NA	8' - 6"	6' - 0" X 7' - 6"	5,000	255
1000	300	15' - 0"	10' - 6"	NA	NA	NA	NA	8' - 6"	6' - 0" X 7' - 6"	5,000	255
1200	500	16' - 6"	12' - 6"	21' - 6"	15' - 0"	19' - 6"	20' - 9" *	9' - 0"	6' - 6" X 7' - 6"	6,600	290
1600	500	16' - 6"	12' - 6"	21' - 6"	15' - 0"	19' - 6"	20' - 0" *	9' - 0"	6' - 6" X 7' - 6"	6,600	290
2000	750	17' - 0"	12' - 6"	22' - 6"	15' - 0"	20' - 0"	20' - 0" *	9' - 0"	7' - 0" X 7' - 6"	7,550	425
2500	1000	18' - 0"	13' - 6"	23' - 6"	16' - 6"	21' - 6"	20' - 0" *	10' - 0"	8' - 0" X 7' - 6"	8,200	435
3000	1000	18' - 0"	13' - 6"	23' - 6"	16' - 6"	21' - 6"	20' - 0" *	10' - 0"	8' - 0" X 7' - 6"	8,200	435
4000	1000 1500**	20' - 0"	16' - 0"	25' - 6"	19' - 0"	23' - 0"	20' - 0"	11' - 0"	10' - 0" X 9' - 0"	10,150	515

24.6.2. Below grade multiple transformer installation 120/208 side by side minimum vault dimensions for multi-services.

LENGTH	13'-6"	13'-6"	14'-0"	15'-0"	15'-0"	16'-6"	16'-6"	17'-0"	18'-0"	18'-0"	20'-0"
-	200i	400i	600i	800i	1000i	1200i	1600i	2000i	2500i	3000i	4000i
WIDTH "A"	9'-6"	9'-6"	9'-6"	10'-6"	10'-6"	12'-6"	12'-6"	12'-6"	13'-6"	13'-6"	16'-0"
WIDTH "B"	7'-6"	7'-6"	7'-6"	8'-6"	8'-6"	9'-6"	9'-6"	9'-6"	10'-6"	10'-6"	12'-0"

WIDTH "A" = Minimum vault requirements for one service panel according to main size

WIDTH "B" = Additional vault requirements for each added service main

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C	EDITORIAL CHANGES	YZZ	EJA	MRF	MRF	04/13/2026	F						
B	EDITORIAL CHANGES	YZZ	JES	FRC	JJP	10/31/2025	E						
A	ORIGINAL ISSUE	-	-	-	-	11/20/2018	D	5745 TABLES MOVED TO FMO	YZZ	FRC	FRC	FRC	07/22/2026

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SDG&E ELECTRIC VAULT REQUIREMENTS AND SPECIFICATIONS

FMO
DM5745.1

24.6.3. Below grade minimum electric vault requirements for 277/480V single 3-phase transformer installation.

CUST. BOARD	480V TRANSF. SIZE	FRONT TO BACK*	WALL TO WALL	ALONG W/ TRANSF. SWITCH INSTALLED ON SIDE WALL		ALONG W/ TRANSF. SWITCH INSTALLED ON END WALL		FLOOR TO CEILING	CEILING EQUIPMENT	TRANSF.	SUMP
SIZE	(KVA)	L LENGTH	W WIDTH	L LENGTH	W WIDTH	L LENGTH	W WIDTH	HEIGHT	OPENING	WEIGHT	CAP.
200	150	13' - 6"	9' - 6"	NA	NA	NA	NA	8' - 0"	4' - 6" X 6' - 6"	3,900	240
400	300	15' - 0"	10' - 6"	NA	NA	NA	NA	8' - 6"	6' - 0" X 7' - 6"	5,000	255
600	500	16' - 6"	12' - 6"	21' - 6"	15' - 0"	19' - 6"	20' - 0"	9' - 0"	6' - 6" X 7' - 6"	6,600	290
800	500	16' - 6"	12' - 6"	21' - 6"	15' - 0"	19' - 6"	20' - 0"	9' - 0"	6' - 6" X 7' - 6"	6,600	290
1000	750	17' - 0"	12' - 6"	22' - 6"	15' - 0"	20' - 0"	20' - 0"	9' - 0"	7' - 0" X 7' - 6"	7,550	425
1200	1000	18' - 0"	13' - 6"	23' - 6"	16' - 6"	21' - 6"	20' - 0"	10' - 0"	8' - 0" X 7' - 6"	8,200	435
1600	1000	18' - 0"	13' - 6"	23' - 6"	16' - 6"	21' - 6"	20' - 0"	10' - 0"	8' - 0" X 7' - 6"	8,200	435
2000	1500	20' - 0"	16' - 0"	25' - 6"	19' - 0"	23' - 0"	20' - 0"	11' - 0"	10' - 0" X 9' - 0"	10,150	515
2500	2000	20' - 0"	16' - 6"	25' - 6"	19' - 6"	23' - 0"	20' - 0"	12' - 0"	10' - 0" X 10' - 0"	17,300	570
3000	2000	20' - 0"	16' - 6"	25' - 6"	19' - 6"	23' - 0"	20' - 0"	12' - 0"	10' - 0" X 10' - 0"	17,300	570
4000	2500 3000**	20' - 0"	16' - 6"	25' - 6"	19' - 6"	23' - 0"	20' - 0"	12' - 0"	10' - 0" X 10' - 0"	17,300	580

24.6.4. Below grade multiple transformer installation 277/480V side by side minimum vault dimensions for multi-services.

LENGTH	13'-6"	15'-0"	16'-6"	16'-6"	11'-0"	12'-0"	18'-0"	20'-0"	20'-0"	20'-0"	20'-0"
-	200i	400i	600i	800i	1000i	1200i	1600i	2000i	2500i	3000i	4000i
WIDTH "A"	9'-6"	10'-6"	12'-6"	12'-6"	12'-6"	13'-6"	16'-0"	16'-6"	16'-6"	16'-6"	16'-6"
WIDTH "B"	7'-6"	8'-6"	9'-6"	9'-6"	9'-6"	10'-6"	10'-6"	12'-0"	12'-6"	12'-6"	12'-6"

WIDTH "A" = Minimum vault requirements for one service panel according to main size
 WIDTH "B" = Additional vault requirements for each added service main

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B	EDITORIAL CHANGES	YZZ	JES	FRC	JJP	10/31/2025	E						
A	ORIGINAL ISSUE	-	-	-	-	11/20/2018	D	5745 TABLES MOVED TO FMO	YZZ	FRC	FRC	FRC	07/22/2026

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SDG&E ELECTRIC VAULT REQUIREMENTS AND SPECIFICATIONS

FMO
DM5745.2

24.6.5. On grade minimum electric vault requirements for 120/208V single 3-phase transformer installation.

CUST. BOARD	208V TRANSF. SIZE	FRONT TO BACK*	WALL TO WALL	ALONG W/ TRANSF. SWITCH INSTALLED ON SIDE WALL		FLOOR TO CEILING	ON GRADE EQUIPMENT OPENING		TRANSF.	SUMP	CLEAR & LEVEL WORKING SPACE IN FRONT OF EQUIPMENT OPENING	
SIZE	(KVA)	L LENGTH	W WIDTH	L LENGTH	W WIDTH	HEIGHT	WIDE	WIDE	WEIGHT	CAP	WIDE	WIDE
200	75	14' - 6"	9' - 6"	14' - 6"	12' - 6"	8' - 0"	7' - 6"	6' - 6"	3,500	240	6' - 0"	7' - 6"
400	150	14' - 6"	9' - 6"	14' - 6"	12' - 6"	8' - 0"	7' - 6"	7' - 6"	3,900	240	6' - 0"	7' - 6"
600	225	16' - 0"	9' - 6"	16' - 0"	12' - 6"	8' - 0"	7' - 6"	7' - 6"	4,200	240	6' - 0"	7' - 6"
800	300	17' - 0"	10' - 6"	17' - 0"	13' - 6"	8' - 0"	8' - 6"	8' - 6"	5,000	255	7' - 0"	8' - 6"
1000	300	17' - 0"	10' - 6"	17' - 0"	13' - 6"	8' - 0"	8' - 6"	8' - 6"	5,000	255	7' - 0"	8' - 6"
1200	500	19' - 6"	12' - 6"	19' - 6"	12' - 6"	9' - 0"	8' - 6"	8' - 6"	6,600	290	7' - 0"	8' - 6"
1600	500	19' - 6"	12' - 6"	19' - 6"	12' - 6"	9' - 0"	8' - 6"	8' - 6"	6,600	290	7' - 0"	8' - 6"
2000	750	20' - 0"	12' - 6"	20' - 0"	15' - 6"	9' - 0"	8' - 6"	8' - 6"	7,550	425	8' - 0"	8' - 6"
2500	1000	21' - 0"	13' - 6"	21' - 0"	16' - 6"	10' - 0"	8' - 6"	8' - 6"	8,200	435	8' - 0"	8' - 6"
3000	1000	21' - 0"	13' - 6"	21' - 0"	16' - 6"	10' - 0"	8' - 6"	8' - 6"	8,200	435	8' - 0"	8' - 6"
4000	100cr... 1500..	23' - 0"	16' - 0"	23' - 0"	19' - 0"	11' - 0"	10' - 0"	10' - 0"	10,150	515	10' - 0"	10' - 0"

24.6.6. On grade multiple transformer installation 120/208V side by side minimum vault dimensions for multi-services.

LENGTH	14'-6"	14'-6"	16'-0"	11'-0"	11'-0"	19'-6"	19'-6"	20'-0"	21'-0"	21'-0"	23'-0"
-	200i	400i	600i	800i	1000i	1200i	1600i	2000i	2500i	3000i	4000i
WIDTH "A"	9'-6"	9'-6"	9'-6"	10'-6"	10'-6"	12'-6"	12'-6"	12'-6"	13'-6"	13'-6"	16'-6"
WIDTH "B"	7'-6"	7'-6"	7'-6"	8'-6"	8'-6"	9'-6"	9'-6"	9'-6"	10'-6"	10'-6"	12'-0"

WIDTH "A" = Minimum vault requirements for one service panel according to main size

WIDTH "B" = Additional vault requirements for each added service main

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A	ORIGINAL ISSUE	-	-	-	-	11/20/2018	D	5745 TABLES MOVED TO FMO	YZZ	FRC	FRC	FRC	07/22/2026

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SDG&E ELECTRIC VAULT REQUIREMENTS AND SPECIFICATIONS

FMO
DM5745.3

24.6.7. On grade minimum electric vault requirements for 277/480V single 3-phase transformer installation.

CUST. BOARD	480V TRANSF. SIZE	FRONT TO BACK*	WALL TO WALL	ALONG W/ TRANSF. SWITCH INSTALLED ON SIDE WALL		FLOOR TO CEILING	ON GRADE EQUIPMENT OPENING		TRANSF.	SUMP	CLEAR & LEVEL WORKING SPACE IN FRONT OF EQUIPMENT OPENING	
SIZE	(KVA)	L LENGTH	W WIDTH	L LENGTH	W WIDTH	HEIGHT	WIDE	WIDE	WEIGHT	CAP	WIDE	WIDE
200	150	14' - 6"	9' - 6"	14' - 6"	12' - 6"	8' - 0"	7' - 6"	7' - 6"	3,900	240	6' - 0"	7' - 7"
400	300	11' - 0"	10' - 6"	17' - 0"	13' - 6"	8' - 6"	8' - 0"	8' - 6"	5,000	255	7' - 0"	8' - 6"
600	500	19' - 6"	12' - 6"	19' - 6"	15' - 6"	9' - 0"	8' - 6"	8' - 6"	6,600	290	7' - 0"	8' - 6"
800	500	19' - 6"	12' - 6"	19' - 6"	15' - 6"	9' - 0"	8' - 6"	8' - 6"	6,600	290	7' - 0"	8' - 6"
1000	750	12' - 0"	12' - 6"	20' - 0"	15' - 6"	9' - 0"	8' - 6"	8' - 6"	7,500	425	8' - 0"	8' - 6"
1200	1000	21' - 0"	13' - 6"	21' - 0"	16' - 6"	10' - 0"	8' - 6"	8' - 6"	8,200	435	8' - 0"	8' - 6"
1600	1000	21' - 0"	13' - 6"	21' - 0"	16' - 6"	10' - 0"	8' - 6"	8' - 6"	8,200	435	8' - 0"	8' - 6"
2000	1500	23' - 0"	16' - 0"	23' - 0"	19' - 0"	11' - 0"	10' - 0"	10' - 0"	10,150	515	10' - 0"	10' - 0"
2500	2000	23' - 0"	16' - 6"	23' - 0"	19' - 6"	12' - 0"	10' - 0"	10' - 0"	17,300	570	10' - 0"	10' - 0"
3000	2000	23' - 0"	16' - 6"	23' - 0"	19' - 6"	12' - 0"	10' - 6"	10' - 0"	17,300	570	10' - 0"	10' - 0"
4000	2500 3000*	23' - 0"	16' - 6"	23' - 0"	19' - 6"	12' - 0"	10' - 6"	10' - 0"	17,300	580	10' - 0"	10' - 0"

24.6.8. On grade multiple transformer installation 277/480V side by side minimum vault dimensions for multi-services.

LENGTH	14'-6"	11'-0"	19'-6"	19'-6"	20'-0"	21'-0"	21'-0"	23'-0"	23'-0"	23'-0"	23'-0"
-	200i	400i	600i	800i	1000i	1200i	1600i	2000i	2500i	3000i	4000i
WIDTH "A"	9'-6"	10'-6"	12'-6"	12'-6"	12'-6"	13'-6"	16'-0"	16'-6"	16'-6"	16'-6"	16'-6"
WIDTH "B"	7'-6"	8'-6"	9'-6"	9'-6"	9'-6"	10'-6"	10'-6"	12'-0"	12'-6"	12'-6"	12'-6"

WIDTH "A" = Minimum vault requirements for one service panel according to main size
 WIDTH "B" = Additional vault requirements for each added service main

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FMO
DM5745.4

5800
CAPACITORS

5800
CAPACITORS

5800 - No FMO standards for this section.

5900

WIRE & SUPPORTS

5900

WIRE & SUPPORTS

5900 - No FMO standards for this section.

6000
SUBSTATION
LOAD FORECASTING

6000
SUBSTATION
LOAD FORECASTING

6000 - No FMO standards for this section.

6100
SECTIONALIZING
& PROTECTION

6100
SECTIONALIZING
& PROTECTION

DM6114 FIELD MAINTENANCE ONLY

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REVISION HISTORY:

09/16/2024: MOVED TO FMO

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A	6114 MOVED TO FMO	JIK	MAK	FRC	KRG	09/16/2024	D						

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SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

UNDERGROUND SERVICE RESTORER

FMO
DM6114

SCOPE

This document provides criteria for the selection and application of 12KV feeder sectionalizing devices on selected high-risk circuits.

PURPOSE

Application of automatic sectionalizing devices for underground circuits (pad-mounted service restorer and PME3 with SCADA) can be beneficial in reducing the number of customers affected by service interruptions. These devices are also helpful in reducing the projected SAIDI by minimizing the impact of a failure of the unfused high molecular polyethylene (HMWPE or PECH in GFMS or unjacketed cross-linked polyethylene (XLPE) cable.

CRITERIA

- A. Circuits chosen for study should meet one or more of the following:
 - 1. A high amount of unfused type HMWPE or XLPE cable as defined by
 - a. Total cable length exceeding one mile or
 - b. Exceeding 20 percent of the total underground cable length
 - 2. Underground outage history exceeding three feeder outages over the last three years regardless of cause.
- B. In addition to the above, the application must be prioritized based on the cost-to-benefit (C/B) ratio analysis in Design Manual section 6145. The projected value (the inverse of the C/B ratio) must be greater than one to justify the additional sectionalizing devices. Alternate methods of project methods of project justification may be allowed by Electric Distribution Planning.

APPLICATION

The circuit under consideration must be examined to ensure that it will meet the switching provisions of Design Manual section 6111 after modification. Service restorers are the preferred device because of the automatic operation and the fact that they can immediately reduce the number of customers affected by an outage. If a service restorer is already in use on a circuit, the PME3 with SCADA should be used where substation SCADA is available or will be available within two years. In cases where the frequency is not as critical, the PME3 with SCADA may be the most economical choice.

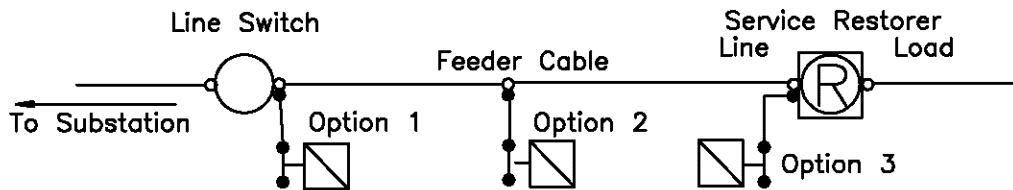
- 1. 600A Padmounted Service Restorer
 - a. Consideration must be made regarding the location and length of the unfused cable segments when locating the service restorer. As a general guide, locate the service to maximize the amount of load on the line side of the device and to maximize the circuit length on load side. The service restorer should be located to protect at least one half of the circuit load. If this is not practical, locate to maximize the isolation of the unfused cable sections.
 - b. A line switch is required immediately ahead of the service restorer for maintenance. This may be an overhead gang operated or hookstick switch, a padmount switch, a handhole switch (On-Off), or a manhole switch (group/On-Off). Manhole switches are acceptable for this application but they are not preferred.

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APPLICATION (continued)

- c. No load should be connected between the service restorer and the line switch immediately ahead. An exception to this rule would be the placement of a single phase transformer that would only provide secondary service for the actuator device within the service restorer. This single phase transformer may tap the feeder at either the switch, the service restorer or in between. Following is an illustrative one-line diagram for the three optional hookups.



Special Note: DM 6121.3.d.1 requires that a fuse request be submitted and approved prior to installation of un-fused transformer stations.

- d. If the service restorer is located so as to protect a purely underground section it shall be set for one test reclosing 5 seconds after the fault, then lockout. Distribution Planning will determine the number of test reclosings for circuits with overhead spans on the load side of the service restorer.
- e. Distribution Planning must be contacted to obtain settings for all protective devices on the circuit.

2. PME3 with SCADA or SCADA Overhead Switch

The PME3 with SCADA should be applied in cases where: 1) A feeder has an existing service restorer and protection (fuse) coordination is not possible. 2) The less expensive SCADA switch will provide adequate protection for the circuit being studied.

- a. If existing subsurface or padmount switchgear is strategically placed for service restoration contact Electric Distribution Standards about SCADA actuator retro-fit. This option can be more economical than other options.
- b. Install SCADA type switches at the midpoint, one-quarter and three-quarter points on the feeder in that order of preference. These may be the new PME3 SCADA switch, SCADA overhead switch, or an existing underground switch retro-fitted with SCADA.
- c. SCADA operated devices may be installed on feeders from current non-SCADA substations where SCADA is not planned within two years. Substations where SCADA is not planned within two years will limit options to automatic protection devices.
- d. Consideration should be given to converting strong tie switches to SCADA.

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	UNDERGROUND SERVICE RESTORER APPLICATION CRITERIA			DATE 1-1-94
				APPD MF/ROJ

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	RELAY AND FUSE COORDINATION TABLES					

RELAY AND FUSE COORDINATION TABLES

FMO
DM6134.1

MINIMUM LINE-TO-GROUND FAULT CURRENT REQUIRED FOR COORDINATION

MINIMUM LINE-TO-GROUND FAULT CURRENT REQUIRED FOR COORDINATION																										
Relay Type	KEARNY OA					S&C SM-4				FUSE				TYPE/SIZE		EOD/SD EJO-1				KB		RTE	FE			
	75	100	125	150	200	65	80	100	125	150	200	80	100	150	200	80	150	150				30				
CO-B	1	*	*	2100	3900	7800	*	*	*	*	3300	5100	6900	*	*	2160	3600	*	2040	3300	*	*				
	2	*	*	*	1500	4800	*	*	*	*	1140	1950	3900	*	*	1830	2700	*	1410	1800	*	*				
	3	*	*	*	1200	3600	*	*	*	*	1410	2340	1980	*	*	1740	2460	*	1290	1350	*	*				
	4	*	*	*	2430	2430	*	*	*	*	*	1980	1800	*	*	1650	2340	*	*	*	*	*				
	5	*	*	*	*	2100	*	*	*	*	*	1800	1800	*	*	1530	2250	*	*	*	*	*				
IAC53	1	*	1350	3300	4800	8400	*	*	2520	4500	6000	7800	*	*	900	2670	3750	*	2700	3750	*	*				
	2	*	*	*	2700	6000	*	*	*	1200	3600	5400	*	*	1980	2850	*	1560	2340	*	*					
	3	*	*	*	1500	5100	*	*	1050	1500	3600	5670	*	*	1830	2670	*	1380	1800	*	*					
	4	*	*	*	1275	4200	*	*	*	1400	2550	2460	*	*	1800	2460	*	1320	1650	*	*					
	5	*	*	*	*	3000	*	*	*	1320	2190	2190	*	*	1710	2400	*	1260	1290	*	*					
CO 1	1	*	*	*	2460	6000	*	*	*	1320	3300	5100	*	*	1980	2940	*	1560	2250	*	*					
	2	*	*	*	1200	4200	*	*	*	1380	2850	2040	*	*	1770	2550	*	1290	1500	*	*					
	3	*	*	*	*	2700	*	*	*	1320	2040	1920	*	*	1650	2400	*	1260	1275	*	*					
	4	*	*	*	*	2100	*	*	*	*	1920	1680	*	*	1560	2280	*	*	*	*	*					
	5	*	*	*	*	1890	*	*	*	*	1680	1680	*	*	1500	2160	*	*	*	*	*					
CO-A1	1	*	*	2100	3900	7500	*	*	*	3300	5400	6600	*	*	2310	3300	*	2430	3300	*	*					
	2	*	*	*	1350	4800	*	*	*	2250	3600	3600	*	*	1830	2700	*	1500	1950	*	*					
	3	*	*	*	3300	3300	*	*	*	1350	2200	1950	*	*	1725	2430	*	*	1330	*	*					
	4	*	*	*	2400	2400	*	*	*	*	1950	1770	*	*	2590	2370	*	*	*	*	*					
	5	*	*	*	*	1950	*	*	*	*	1770	1770	*	*	*	2250	*	*	*	*	*					
IAC51	1	*	1800	2550	3700	6000	*	1500	2100	3300	4200	5400	*	*	1200	2400	3150	*	2700	3200	*	*				
	2	*	*	*	1800	2400	4500	*	*	1200	2100	2760	3600	*	*	1050	2100	2750	*	2100	2400	*				
	3	*	*	*	1200	3600	5000	*	1500	2100	3000	2675	*	*	1000	1950	2675	*	1800	2000	*					
	4	*	*	*	900	2400	2400	*	*	1330	1800	2500	*	*	900	1850	2500	*	1650	1800	*					
	5	*	*	*	*	1450	2100	*	*	1260	1530	2150	*	*	*	1800	2400	*	1500	1700	*					
IT >	1250	1500	2000	2500	3750	1300	1600	2000	2500	3100	3700	650	800	1500	1800	800	1700	2000								

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C							F						
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A	REVISION	-	-	-	JCE	01/01/2000	D						

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	RELAY AND FUSE COORDINATION TABLES								

MINIMUM LINE-TO-GROUND FAULT CURRENT REQUIRED FOR COORDINATION																											
Relay Type	KEARNY QA					S&C SM-4					FUSE					TYPE/SIZE			EOD/SD EJO-1					KB		RTE	FE
	75	100	125	150	200	65	80	100	125	150	200	80	100	150	200	80	150	150	150	2000	2000	550					
CO-8	*	*	*	2700	7200	*	*	*	1950	4050	6000	*	*	1950	2940	*	1425	2250	*	*	*	*					
	*	*	*	*	3900	*	*	*	1680	1300	2400	*	*	1680	2490	*	*	*	*	*	*	*					
	*	*	*	*	2200	*	*	*	1530	*	1920	*	*	1530	2340	*	*	*	*	*	*	*					
	*	*	*	*	1800	*	*	*	*	*	1740	*	*	*	2190	*	*	*	*	*	*	*					
	*	*	*	*	1650	*	*	*	*	*	1650	*	*	*	2100	*	*	*	*	*	*	*					
IAC53	*	*	*	3900	8100	*	*	*	3600	4800	6900	*	*	2190	3000	*	2040	3450	*	*	*	*					
	*	*	*	*	5100	*	*	*	*	1350	3600	*	*	1800	2700	*	1290	1650	*	*	*	*					
	*	*	*	*	2640	*	*	*	*	*	2220	*	*	1650	2430	*	*	*	*	*	*	*					
	*	*	*	*	2040	*	*	*	*	*	1920	*	*	1560	2400	*	*	*	*	*	*	*					
	*	*	*	*	1800	*	*	*	*	*	1740	*	*	*	2280	*	*	*	*	*	*	*					
CO	*	*	*	1170	5400	*	*	*	*	1380	4200	*	*	1800	2670	*	1290	1650	*	*	*	*					
	*	*	*	*	2490	*	*	*	*	*	1920	*	*	1560	2370	*	*	*	*	*	*	*					
	*	*	*	*	1890	*	*	*	*	*	1680	*	*	*	2250	*	*	*	*	*	*	*					
	*	*	*	*	1740	*	*	*	*	*	1650	*	*	*	2100	*	*	*	*	*	*	*					
	*	*	*	*	*	*	*	*	*	*	1630	*	*	*	2100	*	*	*	*	*	*	*					
CO-A1	*	*	*	2850	6900	*	*	*	*	4200	5900	*	*	1950	3000	*	1700	2100	*	*	*	*					
	*	*	*	4200	*	*	*	*	*	*	2700	*	*	1700	2550	*	*	*	*	*	*	*					
	*	*	*	*	2050	*	*	*	*	*	1800	*	*	1500	2350	*	*	*	*	*	*	*					
	*	*	*	*	1700	*	*	*	*	*	*	*	*	*	2200	*	*	*	*	*	*	*					
	*	*	*	*	*	*	*	*	*	*	*	*	*	*	2100	*	*	*	*	*	*	*					
IAC51	*	*	*	3600	6000	*	*	*	3000	3700	5150	*	*	2250	3000	*	2550	3000	*	*	*	*					
	*	*	*	3000	4500	*	*	*	1880	2700	3400	*	*	2000	2700	*	1950	2250	*	*	*	*					
	*	*	*	1650	3600	*	*	*	1320	1920	2700	*	*	1850	2500	*	1650	1900	*	*	*	*					
	*	*	*	1400	2700	*	*	*	*	1600	2300	*	*	1800	2400	*	1500	1750	*	*	*	*					
	*	*	*	1250	2400	*	*	*	*	1470	2100	*	*	1700	2250	*	1350	1500	*	*	*	*					
IT	>	1250	1500	2000	2500	3750	1300	1600	2000	2500	3100	3700	650	800	1500	1800	800	1700	2000	2000	550						
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MINIMUM LINE-TO-GROUND FAULT CURRENT REQUIRED FOR COORDINATION

MINIMUM LINE-TO-GROUND FAULT CURRENT REQUIRED FOR COORDINATION																								
Relay Type	KEARNY QA					S&C SM-4					FUSE					TYPE/SIZE	EOD/SD EJO-1	KB			RTE	FE		
	75	100	125	150	200	65	80	100	125	150	200	80	100	150	200			80	150	150			30	
CO-8	1	*	*	*	6000	*	*	*	*	*	4800	*	*	1740	2700	*	*	*	*	*	*	*		
	2	*	*	*	2100	*	*	*	*	*	1800	*	*	* 2330	2200	*	*	*	*	*	*	*		
	3	*	*	*	*	*	*	*	*	*	*	*	*	* 2100	*	*	*	*	*	*	*	*		
	4	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
	5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
IAC53	1	*	*	*	6400	*	*	*	*	*	4500	6000	*	1980	3000	*	*	*	*	2100	*	*		
	2	*	*	*	3670	*	*	*	*	*	2040	1800	*	1550	2400	*	*	*	*	*	*	*		
	3	*	*	*	1860	*	*	*	*	*	*	*	*	* 2280	2160	2100	*	*	*	*	*	*		
	4	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
	5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
CO 1	1	*	*	*	3750	*	*	*	*	*	2100	*	*	1530	2400	*	*	*	*	*	*	*		
	2	*	*	*	*	*	*	*	*	*	*	*	*	* 2200	2100	*	*	*	*	*	*	*		
	3	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
	4	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
	5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
CO-A1	1	*	*	*	6000	*	*	*	*	*	5250	*	*	1725	2700	*	*	*	*	*	*	*		
	2	*	*	*	1950	*	*	*	*	*	1800	*	*	* 2400	2100	*	*	*	*	*	*	*		
	3	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
	4	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
	5	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
IAC51	1	*	*	1950	3000	5400	*	*	*	*	*	4800	*	2200	3000	*	*	2400	2700	*	*	*		
	2	*	*	*	1650	3750	*	*	*	*	3000	*	*	1950	2700	*	*	1800	1650	*	*	*		
	3	*	*	*	*	2900	*	*	*	*	2400	*	*	1800	2500	*	*	1350	*	*	*	*		
	4	*	*	*	*	2400	*	*	*	*	2100	*	*	1740	2400	*	*	*	*	*	*	*		
	5	*	*	*	*	2100	*	*	*	*	1950	*	*	1700	2300	*	*	*	*	*	*	*		
IT >	1250	1500	2000	2500	3750	1300	1600	2000	2500	3100	3700	650	800	1500	1800	800	1700	2000	550					

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SERVICE RESTORER/FUSE COORDINATION TABLE

FMO
DM6136.1

SCOPE: This standard shows the minimum line to ground fault current required for safe coordination between service restorers and fuses.

Service Restorer Ground Slow Setting Curve		Fuse Type/Size															
		QA															
		15	20	25	30	40	50	60	75	100	125	150	200	30	80	150	
14	18	125	300	400	525	675	875	1050	1500	1975	2725	3300	4800	750	1250	2700	
14	14	250	425	450	575	750	925	1200	1550	2100	2700	3250	5100	825	1350	2700	
14	8	450	600	750	900	1150	1550	1750	2400	3000	3900	4800	7500	850	1800	3600	
14	3	125	225	275	375	525	625	825	1125	1500	1800	2400	3750	700	1050	2100	
14	2	175	300	400	525	650	825	1050	1350	1800	2400	3000	4500	725	1200	2475	
14	K	300	1500	1800	2250	2700	3200	4400	6000	7600	10000	12000	18000	1050	2550	5400	
70	18	*	*	*	*	225	325	450	1050	1725	2325	3000	4650	600	1050	2550	
70	14	*	*	*	225	450	750	975	1450	1950	2475	3150	5100	725	1200	2650	
70	8	*	*	*	600	975	1275	1550	2400	3000	3900	4800	7500	650	1500	3000	
70	3	*	*	*	*	250	375	450	750	1175	1575	2175	3750	550	900	1950	
70	2	*	*	*	*	275	400	550	1075	1575	2175	2925	4500	600	1050	2400	
70	K	*	*	*	*	*	*	*	1800	4500	10000	12000	18000	550	1050	4500	
100	18	*	*	*	*	*	*	325	525	1050	2000	2700	4500	525	750	2325	
100	14	*	*	*	*	*	425	750	1350	1825	2425	3100	5100	700	1150	2625	
100	8	*	*	*	*	600	1050	1425	2250	3000	3900	4800	7500	750	1650	3600	
100	3	*	*	*	*	*	*	375	600	900	1350	1950	3600	525	750	1850	
100	2	*	*	*	*	*	300	425	750	1350	1900	2700	4500	575	875	2250	
100	K	*	*	*	*	*	*	*	*	600	5200	9000	18000	*	650	3300	
140	18	*	*	*	*	*	275	375	600	1350	2100	2850	4500	450	650	2050	
140	14	*	*	*	*	*	*	425	1150	1725	2400	3000	5100	600	1050	2500	
140	8	*	*	*	*	*	450	1200	2100	3000	3900	4800	7500	700	1500	3600	
140	3	*	*	*	*	*	*	*	475	750	1050	1775	3300	*	450	1350	
140	2	*	*	*	*	*	*	*	550	900	1500	2400	4500	400	725	2100	
140	K	*	*	*	*	*	*	*	*	*	825	4200	19500	525	675	2250	
170	18	*	*	*	*	*	*	*	*	600	900	1800	4500	*	600	1650	
170	14	*	*	*	*	*	*	*	750	1500	2100	3000	4900	550	900	2400	
170	8	*	*	*	*	*	*	750	1350	2700	3750	4800	7500	675	1250	3300	
170	3	*	*	*	*	*	*	*	*	675	925	1500	2800	*	600	1500	
170	2	*	*	*	*	*	*	*	*	725	1075	2050	4450	*	675	1800	
170	K	*	*	*	*	*	*	*	*	*	*	1200	13500	*	*	1350	
200	18	*	*	*	*	*	*	*	*	*	775	1350	4200	*	*	1500	
200	14	*	*	*	*	*	*	*	*	1200	2050	2725	4600	*	750	2350	
200	8	*	*	*	*	*	*	*	1500	2550	3650	4500	7500	600	1350	3300	
200	3	*	*	*	*	*	*	*	*	600	850	1350	2700	*	600	1400	
200	2	*	*	*	*	*	*	*	*	600	900	1725	4200	*	650	1725	
200	K	*	*	*	*	*	*	*	*	*	*	1050	8500	*	*	1425	
240	18	*	*	*	*	*	*	*	*	*	*	1200	3400	*	*	1425	
240	14	*	*	*	*	*	*	*	*	750	1725	2700	4600	*	*	2200	
240	8	*	*	*	*	*	*	*	*	2100	3300	4500	7500	*	950	3200	
240	3	*	*	*	*	*	*	*	*	*	750	1250	2600	*	*	1350	
240	2	*	*	*	*	*	*	*	*	*	825	1350	3900	*	*	1500	
240	K	*	*	*	*	*	*	*	*	*	*	*	6000	*	*	*	
280	18	*	*	*	*	*	*	*	*	*	*	1050	2300	*	*	1275	
280	14	*	*	*	*	*	*	*	*	*	1200	2400	4500	*	*	2100	
280	8	*	*	*	*	*	*	*	*	1700	3000	4200	7500	*	*	3000	
280	3	*	*	*	*	*	*	*	*	*	*	1150	2100	*	*	1300	
280	2	*	*	*	*	*	*	*	*	*	*	1225	3000	*	*	1350	
280	K	*	*	*	*	*	*	*	*	*	*	*	1500	*	*	*	

NOTES:

* Will coordinate for all fault current values.

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B	6136 MOVED TO FMO	YZZ	MOV	FRC	FRC	07/14/2026	E						
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SERVICE RESTORER/FUSE COORDINATION TABLE

FMO
DM6136.1

**6200
SYSTEM
ENGINEERING**

**6200
SYSTEM
ENGINEERING**

ALL VERSIONS LISTED IN FMO ARE SUPERSEDED BY THEIR CURRENT VERSION FOUND INSIDE THE ELECTRIC DISTRIBUTION DESIGN MANUAL.

05/22/2026: MOVED TO FMO

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FMO
DM6213

SCOPE

This standard provides the proper single-phase primary transformer voltage selection for boosted and unboosted areas on 12kV distribution circuits.

PURPOSE

This standard was developed to maintain 114 volts minimum (phase to neutral) at the customer's service entrance, based on the Distribution Circuit Profile (Design Standard 6211)

DEFINITIONS

Boosted Area – a physical location on a 12kV circuit served by a booster to provide 7,200 volts from a 12,000/6,930 volt source for proper operation of 7,200 volt transformers.

Boosted Rating – the kVA nameplate rating of 100 or 333 kVA–1Ø and 1875 or 3750 kVA–3Ø.

Booster Ultimate Loading – the maximum allowable peak loading of a booster is established as 100 percent of booster rating.

STANDARD

A. Boosted Area

Transformers rated 7,200 volts should be selected for boosted areas, provided the booster connected kVA will not exceed 90 percent of the booster rating with the kVA additions included.

- When exceeding 90 percent booster rating, Electric Distribution Planning approval is required for 7,200V transformer additions.

B. Unboosted Areas

1. Transformers rated 6,930 volts will always be selected for new installations in unboosted areas.
2. Transformers rated 6,930 volts will always be selected to replace existing 7,200V transformers in unboosted areas more than 1–1/2 miles from the distribution substation.
3. Transformers rated 6,930 volts will always be selected to replace existing 7,200V transformers in unboosted areas less than 1–1/2 miles from the distribution substation, provided the cost associated with converting live front (7,200V) to deadfront (6,930V) transformers is moderate and the interruption of service does not exceed 1 hour for commercial or 6 hours for residential customers. Where a high cost and/or extended outage time for the conversion is required, the replacement use of 7,200V transformers is acceptable.

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TRANSFORMER PRIMARY VOLTAGE SELECTION

FMO
DM6213.1

Example:

Select the proper transformer primary voltage for the addition of 12–25 kVA single-phase transformers in a boosted area served by a 1875 kVA booster with 1400 kVA already connected.

1. Determine the booster loading requiring Electric Distribution Planning approval; 1875 kVA, booster rating (.9) = 1688 kVA
2. Determine total proposed connected kVA on the booster; 1400 kVA, existing + 300 kVA, proposed = 1700 kVA
3. Obtain Electric Distribution Planning approval for the proposed 7,200V transformer additions. Electric Distribution Planning should consider:
 - If the proposed additional transformers will result in the booster exceeding the booster ultimate loading due to actual demand.
 - If a 6,930 volt source should be brought into the area to serve the proposed additional transformers.

References:

1. Design Standard 6211, Distribution Circuit Voltage Profile
2. Service Planning Manual 353, Planned and Requested Outages

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TRANSFORMER PRIMARY VOLTAGE SELECTION

**FMO
DM6213.2**

DM6222 FIELD MAINTENANCE ONLY

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REVISION HISTORY:

09/16/2024: MOVED TO FMO

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APPLICATION OF GROUNDING BANKS

FMO
DM6222

SCOPE

This criteria shall be used for the application of grounding banks. Grounding banks provide a grounded neutral source that is required by load additions which are served by 6.9kV transformers.

DEFINITIONS

A grounding bank installation consists of three-phase transformers connected grounded wye-delta and is used to provide a ground source for the primary neutral wire. The primary voltage rating of the transformers used can be 12 or 6.9kV. The secondary voltage shall be rated 480 volts or higher (see O.H. Standards page 1195).

APPLICATION OF GROUNDING BANKS

A. Why Grounding Banks?

A grounding bank may be installed to serve single-phase load additions using 6.9kV transformers when there are two or fewer grounding banks on a circuit and:

1. Extension of an existing neutral wire, beyond the proper location for a grounding bank, is double the cost of a new grounding bank installation.
2. A neutral connected to an existing grounding bank is available, but additional single-phase load will exceed the recommended kVA limit on the existing grounding bank (see paragraph B.5).

B. Design Considerations

The following lists several design considerations related to the application of grounding banks.

1. The available short-circuit current sensed by a protective device is reduced approximately 100 amps for each grounding bank between the fault location and the substation. To prevent desensitization of the substation ground relays, the number of grounding banks on a circuit is limited to three installations.
2. A grounding bank should be installed at a central location to enable future loads to take advantage of this neutral source. Since there will normally be a maximum of three grounding banks per circuit, each grounding bank should be located to cover one third of the area served by the circuit.

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APPD CVN/ 						

3. The recommended location for a grounding bank is on the unfused portion of a circuit, preferably on the feeder because the load on the grounding bank will be served by an energized neutral source except during times when the circuit is interrupted or the grounding bank has failed.
4. Neutrals established by grounding banks should only be used to serve transformers fed from the same circuit.
5. The following are approved grounding bank installations, allowable connected kVA unbalance between phases and maximum connected kVA loading.

Grounding Bank Installation	Allowable Connected kVA unbalance Between Phases	Maximum Connected kVA Loading (a)
3 – 50 kVA's	150 kVA	1500 kVA
3 – 75 kVA's	225 kVA	2250 kVA

- (a) The maximum connected kVA allowed was set at 10 times the unbalance which a grounding bank may tolerate because the load unbalance on the average circuit is 10 percent.
 - b. For more information on overhead grounding banks, refer to O.H. Standards Page 1195.
 6. Single-phase loads served from a grounding bank should be divided equally among the three phases to balance the total load as much as possible.
- If the amount of unbalance cannot be kept within the limits set above, one of the following must be done:
- a. Extend the neutral from the substation and remove the grounding bank. This alternative is recommended if there is significant load growth potential in the area.
 - b. Serve part of the load with 12kV single-phase transformers. Use enough 12kV transformers to reduce the amount of 6.9kV connected kVA below the recommended limit.
 - c. Extend the neutral from another grounding bank, either new or existing, and transfer some 6.9kV load to this neutral. These neutrals are not to be connected to each other.

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PRIMARY CONDUCTOR COST COMPARISON

FMO
DM6241

SCOPE

This standard uses graphic representation to illustrate the total owning cost (installation plus losses) of different conductor sizes operating at specific load levels. The information presented in this standard is supplemental to Design Standard 5923, "Preferred UG Cable Installation Criteria".

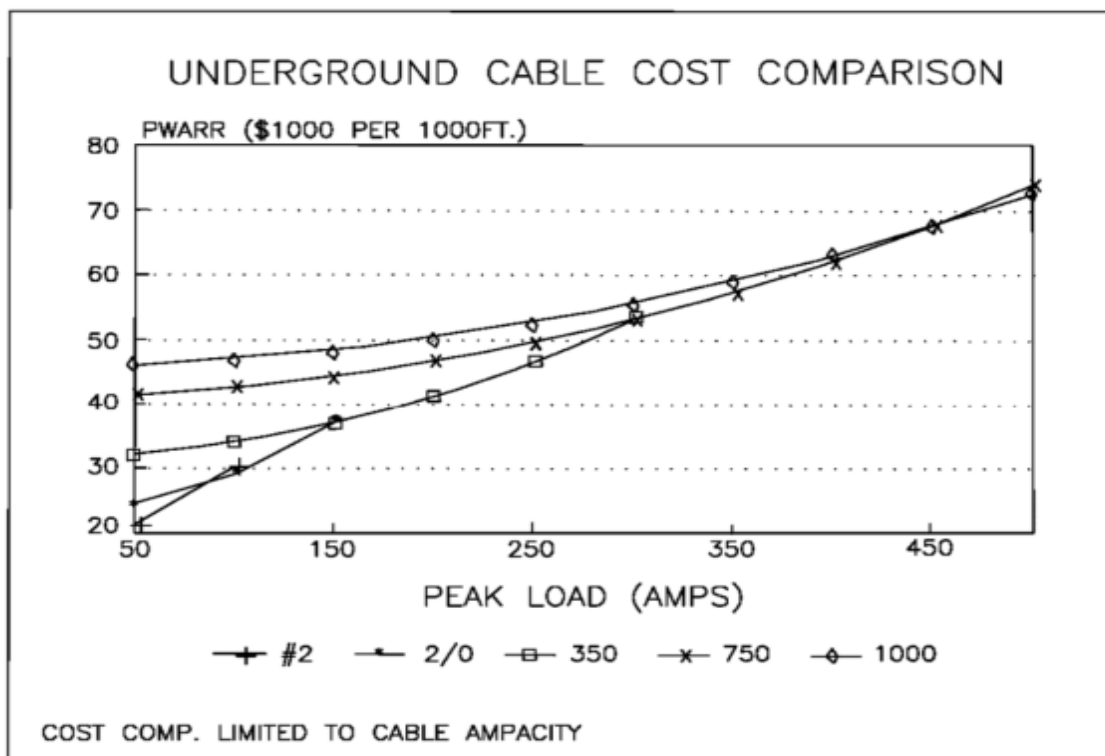
PURPOSE

This standard was prepared so District Engineering personnel would be able to select the least costly conductor size based on the amount of load which the conductor would serve. The graphs also make it possible for the district engineer to determine the cost penalty associated with installing a larger conductor than necessary to provide adequate tie capacity.

CRITERIA

The cost illustrated in the graphs below represent the PWARR to install 1000 feet of conductor plus the demand and energy charges associated with distribution system losses. In addition to the conductor cost the Underground Cable Cost Comparison includes the cost of connectors while the Overhead Conductor Cost Comparison includes the cost of poles, crossarms and anchors.

The graphs were constructed assuming the peak load is constant over the physical life of the conductor (20 years for UG, 30 years for OH). An average peak load to be expected over the life of the conductor must be calculated prior to using the graphs if the peak load is not constant (e.g. due to load growth, specific load additions, etc.).



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C							F						
B	6241 MOVED TO FMO	YZZ	FRC	FRC	FRC	07/17/2026	E						
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PRIMARY CONDUCTOR COST COMPARISON

FMO
DM6241.1

The following constants and assumptions were used to develop the graphs:

1. LACC UG = 16.7% OH = 16.13%
2. Physical Life UG = 20 yrs OH = 30 yrs
3. Energy Charge UG = 4.62¢/kWh OH = 5.44¢/kWh
4. Demand Charge UG = \$97.63/kW OH = 112.5/kW
5. Loss Factor = 0.25
6. Peak Responsibility Factor = 0.80
7. Construction Cost Contingencies = 20%
8. Underground Conductor Parameters:

3-1/c #2 PECN-PEJ	PWARR = \$18,042/1000'	R = .3339 ohms/1000'
3/c #2/0 PECN-PEJ	PWARR = \$22,656/1000'	R = .1663 ohms/1000'
3/c 350 XLPECN-PEJ	PWARR = \$31,504/1000'	R = .0649 ohms/1000'
3/c 750 XLPECN-PEJ	PWARR = \$41,225/1000'	R = .0345 ohms/1000'
3/c 1000 XLPECN-PEJ	PWARR = \$45,625/1000'	R = .0286 ohms/1000'
9. Overhead Conductor Parameters:

3/0 AWG ACSR/AW	PWARR = \$25,726/1000'	R = .1500 ohms/1000'
336 AWG ACSR/AW	PWARR = \$35,335/1000'	R = .0630 ohms/1000'
636 AWG ACSR/AW	PWARR = \$44,633/1000'	R = .0330 ohms/1000'
10. The book life, which is usually the physical life, is 28 years for UG cable and 36 years for OH conductor. PWARR figures used in this standard incorporated these book lives. However, the energy and demand charges used in this standard reflect historical conductor performance, 20 years for UG cable and 30 years for OH conductors.

The table below present the optimum conductor loading for each conductor size in tabular form:

Underground Cable Size	Optimum Conductor Peak Loading
3-1/c #2	0 - 84 amps
3/c #2/0	85 - 151 amps
3/c 350	152 - 290 amps
3/c 750	291 - 445 amps
3/c 1000	> 445 amps

overhead Cable Size	Optimum Conductor Peak Loading
3/0	0 - 151 amps
336	152 - 254 amps
636	> 254 amps

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C							F						
B	6241 MOVED TO FMO	YZZ	FRC	FRC	FRC	07/17/2026	E						
A	REVISION	-	-	-	CVN	01/01/1989	D						

**SHEET
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Information Removed

SDG&E ELECTRIC DISTRIBUTION DESIGN MANUAL FIELD MAINTENANCE ONLY

PRIMARY CONDUCTOR COST COMPARISON

**FMO
DM6241.3**

ALL VERSIONS LISTED IN FMO ARE SUPERSEDED BY THEIR CURRENT VERSION FOUND INSIDE THE ELECTRIC DISTRIBUTION DESIGN MANUAL.

07/18/2025: MOVED TO FMO

REV	CHANGE	DR	BY	DSN	APV	DATE	REV	CHANGE	DR	BY	DSN	APV	DATE
C							F						
B							E						
A	ORIGINAL ISSUE	YZZ	FRC	FRC	FRC	07/18/2025	D						

FMO
DM6242

SCOPE

This standard provides a method of evaluating various alternatives so that the most economical one is identified. The advancement of an overload project to improve reliability is also discussed. For the latest calculation tools used to determine the present value of electric distribution projects, contact Distribution Planning.

PURPOSE

Present Worth of Annual Revenue Requirements (PWARR) has been selected by the Financial and Economic Analysis section as the appropriate analytical tool for distribution engineering projects. This is because it measures the total impact of a project on SDG&E's customers given the regulated environment of the utility.

DEFINITIONS

LACC (Levelized Annual Capital Cost) – A factor applied to the installed equipment costs to account for the annual levelized depreciation, return on investment, income taxes, property taxes and salvage.

A/P,n – Converts a present value into an annual series of payments over n years. Refer to the Economic Assumptions Manual, Table 2-1, for the current value.

P/A,n – Provides the present value of an annual series of payments made for n years. Refer to the Economic Assumption Manual, Table 2-1, for the current value.

P/F,n – Provides the present value of a future payment made n years from today. Refer to the Economic Assumption Manual, Table 2-1, for the current value.

Inflation Factor – Accounts for the rise in the price of goods and services over n years.

CRITERIA

The capital portion of Equation 1 below converts the equipment installed cost (Cost) into an annual series using the LACC Factor to account for taxes and return on investment. Then it sums all these payments into a present value at the time of construction using the P/A factor. In contrast, the O&M portion accounts for those non-capitalized expenditures which are included at the time of installation (O&M) and so the LACC and P/A factors are not applied.

$$PWARR = [(Inflation Factor)(P/F,n)][(Cost)(LACC)(P/A,n)+(O\&M)] \quad \text{Equation 1}$$

$$Inflation Factor = (1+i)^n \quad \text{Equation 2}$$

where: i = rate of inflation

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APPLICATION

PWARR analysis is used to compare alternative construction projects economically. Normally there are benefits associated with each project which have not been assigned a dollar amount and, therefore have not been considered. When the PWARR of one alternative is within 5 percent of another alternative it is appropriate to consider unassigned benefits (i.e. improvements in customer service, sensitivity to changes in input variables, lowest installed cost, etc.) in the decision.

A typical application of the PWARR analysis is shown in Example 1. It considers delaying the construction of a new circuit for two years by increasing tie capacity, thus allowing a load transfer to occur. The alternative is to construct the new circuit next year. Although the lives of the two alternatives are not the same (one ends in 28 years, the other 30), the Finance and Economic Analysis section feels Equation 1 provides a good approximation provided the difference in lives does not exceed 5 years.

Example 1

One feeder in a 4-EB5" duct is rated at 475 amps but has a projected load of 500 amps next year. To eliminate the projected overload consider shedding 100 amps to an adjacent circuit by constructing a tie next year for \$75k. This will delay having to construct a new circuit, at a cost of \$450k for an additional 2 years. The alternative is to construct the new circuit next year. Which alternative is the least costly considering all costs were provided in next year's dollars?

The following factors were obtained from the economic Assumptions Manual:

$$\begin{aligned} \text{LACC} &= 0.167, \text{ FERC account E367 (book life} = 28 \text{ yrs)} \\ \text{P/A, } 28 &= 8.2217 \\ \text{P/F, } 2 &= 0.8029 \\ \text{A/P, } 2 &= 0.5886 \\ i &= 5\% \end{aligned}$$

ALTERNATIVE 1: Construct a tie next year and defer the new circuit 2 years.

$$\text{Inflation Factor} = (1.05)^2 = 1.1025$$

$$\text{Construct tie PWARR} = (75k)(0.167)(8.2217) = \$102,976$$

$$\begin{aligned} \text{Construct circuit 2 yrs later PWARR} &= (1.1025)(.8029)(450k)(0.167)(8.2217) \\ &= \$546,929 \end{aligned}$$

$$\text{Total Cost } \$649,905$$

ALTERNATIVE 2:

$$\text{Construct circuit next year PWARR} = (450k)(0.167)(8.2217) = \$617,861$$

Conclusion Alternative 2 is approximately 5% less expensive and it should be selected unless there are sufficient unassigned benefits to favor alternative 1.

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Example 2

Consider advancing the construction of a new circuit 2 years to achieve an annual reliability benefit of \$100,000. The circuit cost is the same as in Example 1. Is this cost effective?

$$\text{Construct line next year} - (450k)(0.167)(8.2217) = \$617,861$$

$$\text{Construct line 2 yrs later} - (1.1025)(0.8029)(450k)(0.167)(8.2217) = \$546,929$$

$$\text{PWARR of advancement} = 617,861 - 546,929 = \$70,932$$

$$\text{C/B ratio} = (70,929)(A/P_2)/100,000 = 0.4175$$

Conclusion: It is cost effective to move the project ahead 2 years.

Example 3

Consider the effect of adding O&M expenditures to the construction in Example 1. O&M associated with constructing the new line is \$75k, \$15k for constructing the tie.

ALTERNATIVE 1:

$$\text{Construct tie line next year} \quad \text{PWARR} = \$102,976 + \$15,000 = \$117,976$$

$$\text{Construct ckt 2 yrs later} \quad \text{PWARR} = \$546,929 = (75k)(1.1025)(.0829) = \$613,319$$

$$\text{Total cost} = \$731,295$$

ALTERNATIVE 2:

$$\text{Construct new circuit next year} \quad \text{PWARR} = \$617,861 + \$75,000 = \$692,861$$

Conclusion: Alternative 2 is still approximately 5% less expensive and should be selected unless there are sufficient unassigned benefits to favor alternative 1.

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